

Lecture #16

OUTLINE

The Bipolar Junction Transistor

- Narrow-emitter and/or narrow-collector
- Ebers-Moll model
- Base-width modulation, Early voltage

Reading: Chapter 11.2

Narrow-Emitter and Narrow-Collector

$$I_{En} = qA \frac{D_E}{L_E} n_{E0} \frac{\cosh(W_E' / L_E)}{\sinh(W_E' / L_E)} (e^{qV_{EB} / kT} - 1)$$

$$I_{Cn} = -qA \frac{D_C}{L_C} n_{C0} \frac{\cosh(W_C' / L_C)}{\sinh(W_C' / L_C)} (e^{qV_{CB} / kT} - 1)$$

$$I_E = qA \left[\left(\frac{D_E}{W_E'} n_{E0} + \frac{D_B}{L_B} p_{B0} \frac{\cosh(W / L_B)}{\sinh(W / L_B)} \right) (e^{qV_{EB} / kT} - 1) - \left(\frac{D_B}{L_B} p_{B0} \frac{1}{\sinh(W / L_B)} \right) (e^{qV_{CB} / kT} - 1) \right]$$

$$I_C = qA \left[\left(\frac{D_B}{L_B} p_{B0} \frac{1}{\sinh(W / L_B)} \right) (e^{qV_{EB} / kT} - 1) - \left(\frac{D_C}{W_C'} n_{C0} + \frac{D_B}{L_B} p_{B0} \frac{\cosh(W / L_B)}{\sinh(W / L_B)} \right) (e^{qV_{CB} / kT} - 1) \right]$$

Performance Parameters (revisited)

$$\gamma = \frac{1}{1 + \frac{n_{iE}^2}{n_{iB}^2} \frac{D_E}{D_B} \frac{N_B}{N_E} \frac{W}{L_E}} \leftarrow \text{Replace with } W_E \text{ if short emitter}$$

$$\alpha_T = \frac{1}{1 + \frac{1}{2} \left(\frac{W}{L_B} \right)^2}$$

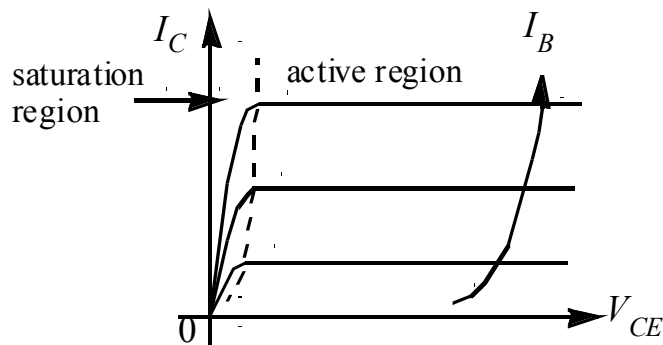
$$\alpha_{dc} = \frac{1}{1 + \frac{n_{iE}^2}{n_{iB}^2} \frac{D_E}{D_B} \frac{N_B}{N_E} \frac{W}{L_E} + \frac{1}{2} \left(\frac{W}{L_B} \right)^2}$$

$$\beta_{dc} = \frac{1}{\frac{n_{iE}^2}{n_{iB}^2} \frac{D_E}{D_B} \frac{N_B}{N_E} \frac{W}{L_E} + \frac{1}{2} \left(\frac{W}{L_B} \right)^2}$$

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Ebers-Moll Model



The Ebers-Moll model is a **large-signal** equivalent circuit which describes both the active and saturation regions of BJT operation.

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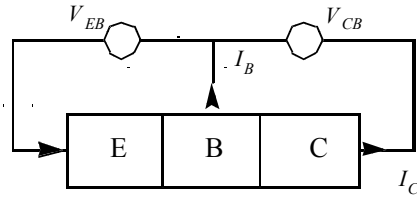
I_C is driven by two forces, V_{EB} and V_{CB} .

If only V_{EB} is applied ($V_{CB} = 0$):

$$I_E = I_{F0} (e^{qV_{EB}/kT} - 1)$$

$$I_C = \alpha_F I_{F0} (e^{qV_{EB}/kT} - 1)$$

$$I_B = (1 - \alpha_F) I_{F0} (e^{qV_{EB}/kT} - 1)$$



If only V_{CB} is applied ($V_{EB} = 0$): :

$$I_C = -I_{R0} (e^{qV_{CB}/kT} - 1)$$

$$I_E = -\alpha_R I_{R0} (e^{qV_{CB}/kT} - 1)$$

$$I_B = I_{R0} (1 - \alpha_R) (e^{qV_{CB}/kT} - 1)$$

α_R : reverse common base gain
 α_F : forward common base gain

In the general case, both V_{EB} and V_{CB} are non-zero:

$$I_C = \alpha_F I_{F0} (e^{qV_{EB}/kT} - 1) - I_{R0} (e^{qV_{CB}/kT} - 1)$$

I_C : C-B diode current + fraction of E-B diode current that makes it to the C-B junction

$$I_E = I_{F0} (e^{qV_{EB}/kT} - 1) - \alpha_R I_{R0} (e^{qV_{CB}/kT} - 1)$$

I_E : E-B diode current + fraction of C-B diode current that makes it to the E-B junction

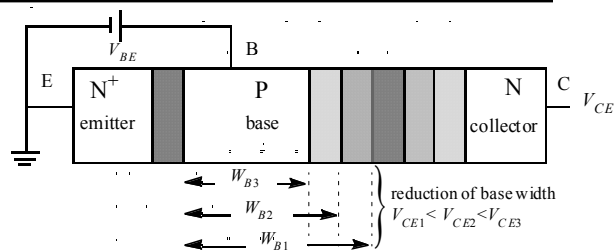
Reciprocity Relationship

$$\alpha_F I_{F0} = \alpha_R I_{R0} \equiv qA \frac{D_B}{L_B} \frac{p_{B0}}{\sinh(W/L_B)}$$

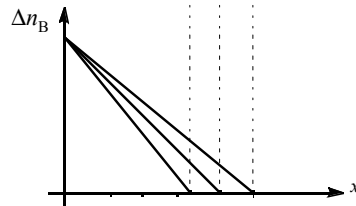
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Base-Width Modulation



$$\beta_{dc} = \frac{1}{\frac{n_{iE}^2}{n_{iB}^2} \frac{D_E}{D_B} \frac{N_B}{N_E} \frac{W}{L_E} + \frac{1}{2} \left(\frac{W}{L_B} \right)^2}$$



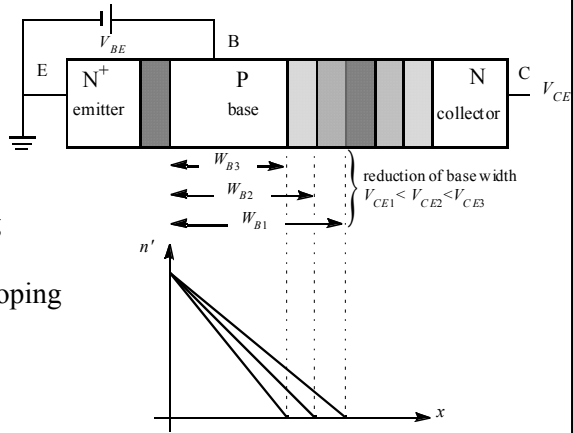
How can we reduce the base-width modulation effect?

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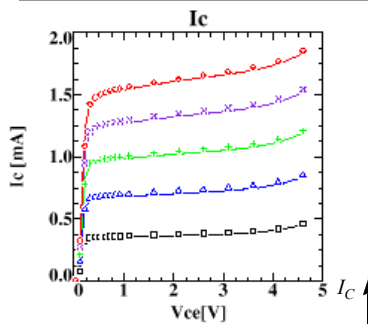
The base-width modulation effect is reduced if we

- (A) Increase the base width,
- (B) Increase the base doping concentration, N_B , or
- (C) Decrease the collector doping concentration, N_C .



Which of the above is the most acceptable action?

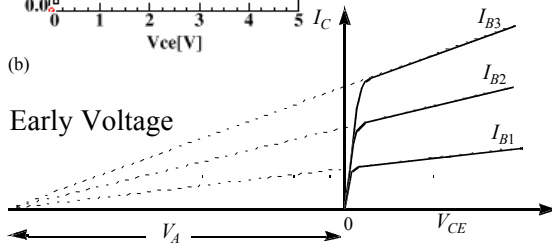
Early Voltage



Output resistance :

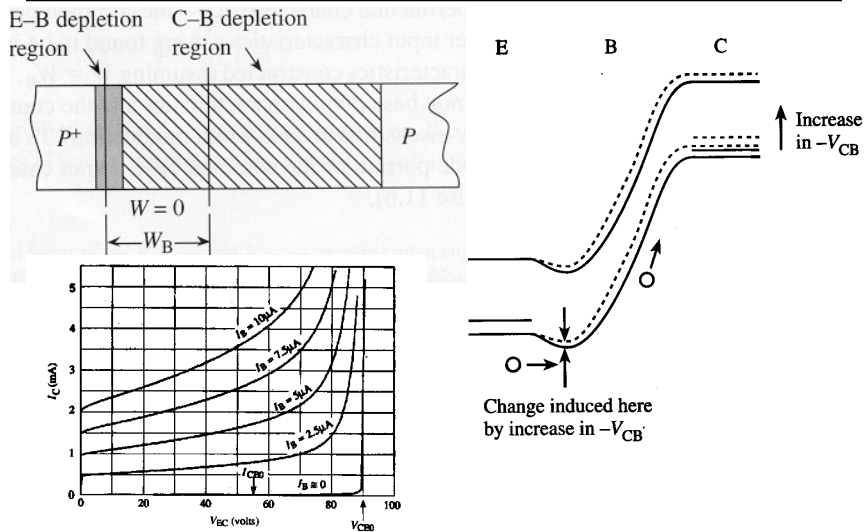
$$r_o \equiv \left(\frac{\partial I_C}{\partial V_{CE}} \right)^{-1} = \frac{V_A}{I_C}$$

(b) V_A : Early Voltage



A large V_A (i.e. a larger r_o) is desirable

Punchthrough



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Summary: BJT Performance Requirements

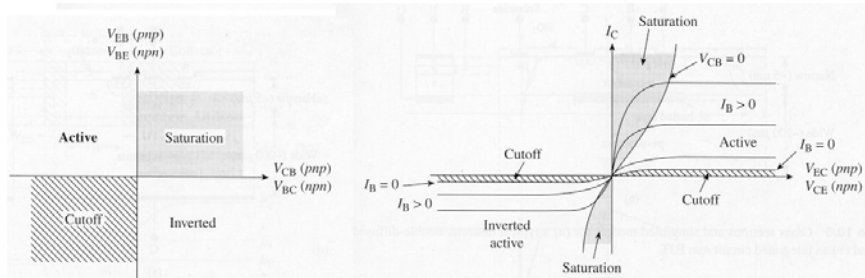
- **High gain** ($\beta_{dc} \gg 1$)
 - One-sided emitter junction, so emitter efficiency $\gamma \approx 1$
 - Emitter doped much more heavily than base ($N_E \gg N_B$)
 - Narrow base, so base transport factor $\alpha_T \approx 1$
 - Quasi-neutral base width \ll minority-carrier diffusion length ($W \ll L_B$)
 - **I_C determined only by I_B** ($I_C \neq$ function of V_{CE}, V_{CB})
 - One-sided collector junction, so quasi-neutral base width W does not change drastically with changes in V_{CE} (V_{CB})
 - Based doped more heavily than collector ($N_B > N_C$)
- $(W = W_B - x_{nEB} - x_{nCB}$ for PNP BJT)

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Review: Modes of Operation

Common-emitter output characteristics (I_C vs. V_{CE})



Note that $\beta_{dc} = \frac{I_C}{I_B}$ is lower for inverted mode operation. Why?